

# Beam Quality and Stability of PAF Systems

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## The ideal polarimetric beamformer should

- provide maximum sensitivity
- preserve polarimetric properties of observed signal
- $\rightarrow$  optimal beamformer

# **Other concerns (a.o.)**

- polarimetric behavior over FoV
- side lobe level
- beam symmetry

# $\rightarrow$ beam shaping using constraints



With orthogonally polarized far field reference sources

- optimal
- max-SNR (signal-to-noise)
- max-SLNR (signal-to-leakage-and-noise)
- correction for imperfect reference sources

With unpolarized far field reference source

- eigenvector method (with bi-scalar correction)
- bi-scalar

# **Green: sensitivity equivalent to optimal method**

#### **Generic model of a phased array** Ivashina, Maaskant & Woestenburg, IEEE AWPL, 2008 Ivashina et al., IEEE TAP, Jun 2011





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#### **Optimal polarimetric calibration (1)** Warnick et al., IEEE TAP, accepted 2011

$$\mathbf{v}_{u}, \mathbf{v}_{v}$$
 voltage response to pure *u*- or *v*-polarized signal

Assume:  $\mathbf{V} = [\mathbf{v}_{\mu}, \mathbf{v}_{\nu}]$  is known

BF output covariance matrix:  $\mathbf{W}^{H}(\mathbf{R}_{s} + \mathbf{R}_{n})$  W

where  $\mathbf{W} = [\mathbf{w}_1, \mathbf{w}_2]$ 

 $\boldsymbol{\mathsf{R}}_{_{\scriptscriptstyle \mathsf{C}}}$  is the signal covariance matrix

**R**<sub>n</sub> is the noise covariance matrix

We want to: 1. minimize the noise:  $\operatorname{argmin}_{W} \operatorname{tr}(W^{H} \mathbb{R}_{P} W)$ 

2. preserve polarization:  $\mathbf{W}^{H}\mathbf{V} = \mathbf{I}$ 

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#### **Steps to solution**

- Reformulate using Lagrange multipliers
- Take derivatives and set them to zero
- Use contraint to find Lagrange multipliers

# Solution

$$\mathbf{W} = \mathbf{R}_{n}^{-1} \mathbf{V} (\mathbf{V}^{H} \mathbf{R}_{n}^{-1} \mathbf{V})^{-1}$$

## Interpretation

- Maximum sensitivity beam former
- Correction for optimal polarimetric fidelity

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Optimal method requires

- generally unavailable orthogonally polarized ref. sources
- polarimetric processing (incl. 2N frontend correlator)
- $\rightarrow$  practical systems exploit bi-scalar processing
  - separate treatment of both polarizations
  - reduces complexity of processing system
  - relies on intrinsic polarimetric quality of antennas
  - possibly sacrifices some sensitivity

# **Question: how bad is this?**

# **Example:** Aperture Tile in Focus

PAF for WSRT, increases survey speed 25x

#### key specs •

Frequency range 300 MHz Instantaneous bandwidth < 55 K System temperature Aperture efficiency Polarization Simultaneous beams Field of view Reflectors

1000 – 1750 MHz

75% dual linear 37 dual pol  $8 \text{ deg}^2$ 12 x 25 m



#### Beam spec: 1% error at HPBW rel. to main beam



#### **Filling the FoV** Ivashina et al., URSI GASS, Aug 2011



EM-simulation of APERTIF prototype for 37 beams

left: compound beams in x-polarization

right: beam center locations with indices



#### **Sensitivity comparison** Wijnholds et al., URSI GASS, Aug 2011

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- EM-simulation of APERTIF prototype for 37 pointings
- Sensitivity loss only 4%
- Recoverable at cost of half the bandwidth



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left: correlation BF output signals for optimal BF

right: correlation BF output signals for bi-scalar BF

Bi-scalar method relies on polarimetric quality of antennas



## Measured dominant eigenvectors Wijnholds et al., URSI GASS, Aug 2011

- measurement on unpolarized source
- amplitudes of elements of two dominant eigenvectors
- 2% sensitivity loss due to ignoring cross-pol (4% in sims)
- -28 dB cross-pol level (sims typically -45 dB)
- acceptable for actual system



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# **Error analysis**



- Beamformer equation:  $y(t) = \mathbf{w}^{H}(\mathbf{\theta}) \mathbf{v}(t)$ 
  - $\mathbf{w}^{H}(\mathbf{\theta})$  weight vectors parameterized by  $\mathbf{\theta}$
  - $\mathbf{v}(t)$  receiving element output voltages
  - y(t) beamformer output voltage
- $\boldsymbol{\theta}$  depends on element response and noise covariance
- assumed parameter covariance models:
  - for calibration: Cramer-Rao bound
  - for drift: independent parameter variation
- standard error propagation formula

 $var(y) = (\partial y / \partial \boldsymbol{\theta}^{\mathsf{T}}) \operatorname{cov}(\boldsymbol{\theta}) (\partial y / \partial \boldsymbol{\theta}^{\mathsf{T}})^{\mathsf{T}}$ 

# **Propagation of calibration errors**



- SNR = 200
- bi-scalar BF
- constraint:
   beam peak
   fixed (selfcal)
- SNR of 200
   needed to
   satisfy beam
   requirement
   for APERTIF

# Propagation of drift errors (on axis) AST(RON

- 2% rel. error
- bi-scalar BF
- constraint:
   beam peak
   fixed (selfcal)
- 2% variations
   well within acceptable tolerances





standard deviation

x 10<sup>-3</sup>

#### **Element patterns on the sky** Van Cappellen, AJDI, 27 Mar 2008



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# Propagation of drift errors (off axis) AST(RON

- 2% rel. error
- bi-scalar BF
- constraint:
   beam peak
   fixed (selfcal)

max 2%
 variation

 acceptable to
 satisfy beam
 spec APERTIF





standard deviation

-3

x 10<sup>-3</sup>

# Measured drift using apex-source

- 5 min observation at 1441.5 MHz
- gain calibrated using first 10 s
- < 1% variation after 5 min  $\rightarrow$  10 15 min update rate?



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- Good progress on PAF analysis
  - sims and measurements give similar results
  - wide range of calibration methods available
  - comparison between methods possible
  - error propagation analysis available
- Application to APERTIF system
  - only 2% (sims: 4%) sensitivity loss bi-scalar BF
  - -28 dB cross-pol level bi-scalar BF acceptable
  - calibration measurement should have SNR of 200

- 10 - 15 min calibration update interval seems ok CalIm, Manchester (UK), 25 July 2011 - 19 -