

#### WP2.2 CoDR PAF Concepts

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# **PAF sub-system review**









# **Optics/antenna considerations**



- 1. f/D
- 2. FoV de-rotation
- 3. Reflector shaping

# f/D



- Moderate f/D  $\sim$  0.4-0.5 is important to minimizing PAF cost
  - Number of PAF elements  $\alpha$  (f/D)<sup>2</sup> for given FoV
  - Good aperture efficiency
- Consistent with Pathfinder and PrepSKA dish activities
  - Front-fed single reflector
  - Offset-fed dual reflector
- Can be difficult to achieve with small blockage in other configurations





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ASKAP



- For high dynamic range, beams must be stable wrt sources whilst integrating in the visibility domain
- Difficult to resolve in image formation
  - Calibration, storage and processing
- Altaz mount + 3rd axis to rotate reflector and feed (eg ASKAP)
- Equatorial mounts (eg WRST)
  - Latitude dependent SKA
- Altaz with electronic beam scan whilst maintaining beam shape

#### FoV de-rotation





- Front-fed single reflector
  - 3<sup>rd</sup> axis has been done (ASKAP)
- Offset-fed dual reflector
  - 3<sup>rd</sup> axis is more difficult
  - Electronic beam scan
    - tertiary pattern must retain shape
    - primary and secondary spillover will rotate wrt sources, so must be small



# Reflector shaping and survey speed





average(
$$\sum_{\text{pointings}} \operatorname{Sen}_{x,y}^{2}(\Omega - \Omega_{\text{pointing}})) = \frac{1}{\partial \Omega} \int_{all \Omega} d\Omega \operatorname{Sen}_{x,y}^{2}(\Omega)$$

$$\Rightarrow$$
 Survey speed  $\propto \int_{all \Omega} d\Omega \operatorname{Sen}^2(\Omega)$ 

# **Reflector shaping**



DSEx SSFOV=32.8 deg<sup>2</sup> S<sub>max</sub>=2.68 m<sup>2</sup>/K S<sup>2</sup><sub>eff</sub>=237 DSEx SSFOV=15.6 deg<sup>2</sup> S<sub>max</sub>=3.11 m<sup>2</sup>/K S<sup>2</sup><sub>eff</sub>=150 deg<sup>2</sup> m<sup>4</sup>/K<sup>2</sup> 3FOV=21 deg<sup>2</sup> S<sub>max</sub>=2.66 m<sup>2</sup>/K S<sup>2</sup><sub>eff</sub>=148 deg<sup>2</sup> m<sup>4</sup>/K<sup>2</sup>







#### **Optics/antenna summary**



- Optics/antennas is important
  - Survey speed / cost
  - Achieving high dynamic range
  - Upgradability of SKA
- Particular concerns
  - FoV rotation impact on dynamic range
  - Unshaped reflectors preferred for performance/cost and future FoV expansion

# PAF Feed Array Concepts









Chequerboard

Vivaldi

Dipole

# Chequerboard PAF overview





- Connected array concept
  - Bandwidth enhanced by flow of conduction current between elements
- Dual-polarized self-complementary patches over groundplane
  - Moderately wideband 2.5:1
  - ~377ohm active impedance
- Potential advantages of planar structure •
  - Integration with low noise amplifiers
  - Cost
  - Other performance aspects eg polarization

# Chequerboard PAF construction







# Chequerboard PAF active balun

Patch





# Chequerboard PAF LNA design







- Discrete components
- Avago ATF 35143 PHEMT FETs
- ~300 ohm differential input Zin and noise source Zopt
- Stable on the array
- Noise parameter estimation from measurements (1/2 and full LNA)

#### **Chequerboard PAF Trec**







- Array modelling
  - Consistent with recent measurements on first 188-element ASKAP PAF
  - LNA noise parameters estimated from measurements
  - Enhanced chequerboard (ASKAP 2 above) with same LNA

# Vivaldi PAF

- Vivaldi array
  - Well characterized element
  - Easy design for 2.5:1 bandwidth
  - Easy design for 50ohm single-ended LNAs
  - High technology readiness level
- Eg APERTIF
  - 121 element dual polarized Vivaldi array, 1 1.8 GHz
  - Laser-cut aluminum plates
  - Microstrip balun on RO4003
  - Overall radiation efficiency ~98.5%
  - Temperature stabilized at 7 °C



VII OMETOE ADDI

10 cm

# **APERTIF LNA**



Room temperature LNA Tmin ~35 K Discrete components





Improved design with Tmin~25K has been prototyped



#### **APERTIF PAF**



#### Aperture array



- Tsys ~50K as aperture array and 68K as PAF (nap=75K)
- Good agreement between modeling and measurement
- Tsys ~ 55K expected for final APERTIF PAF

# Active Vivaldi PAF



- DRAO/UCL effort aimed at reducing Vivaldi loss ٠
- Thicker Vivaldi elements (5mm) ٠
- LNA integrated in element (milled cavity) ٠
- **Reduce dielectric** ٠
- Use of Tmin 20K single-ended LNAs ٠



|                                   | Current Prototype | Final APERTIF |
|-----------------------------------|-------------------|---------------|
| Antenna losses                    | 6                 | 6             |
| LNA + second stage                | 40                | 28            |
| Noise coupling / active impedance | 9                 | 8             |
| Spillover                         | 10                | 10            |
| Sky noise                         | 3                 | 3             |
| Total                             | 68                | 55            |

APERTIF Tsys budget at 1.4GHz Exploring the Universe with the world's largest radio telescope

# **Dipole PAF**





- BYU/NRAO collaboration
- Dual-polarized `Kite' dipole
- Well characterized element
- Tsys 22K target (35K has been measured)
- ηap 70%
- 1.4:1 bandwidth (1dB)

# Dipole PAF LNAs







- LNAs in cryostat (stainless steel transition to ambient dipole)
- Single-ended LNAs (balun in dipole) with 50ohm impedance
- Optimized active noise match

# Fully cooled PAFs





- Cornell study
- Dipoles and LNA cryogenically cooled by two-stage system
- Thermal load modeling
- 91 element 1.4m dia PAF for Arecibo would require 4 CTI1020 coolers

# Conclusions



- PAF principles and capability demonstrated
  - Modelling
  - Low noise ambient temperature LNAs
  - Dense arrays
  - Cryogenic cooling
  - SKA1 0.45-3GHz could be covered with two PAFs
  - Emerging flexible new technology for radioastronomy
- PAF optimization
  - Optimizations required in FOV, optics, frequency range, processing
- PAF key issues
  - Dynamic range budget
  - Astronomy/cost optimization



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