SKACH

The variable MID-band 6 filter: a key component for the MID-band 6/multi-band receiver (Work Package 2360)



Haute Ecole Spécialisée de Suisse occidentale

Fachhochschule Westschweiz

University of Applied Sciences Western Switzerland





Toward Mid6





















Heterodyne



Pros:

- ✓ Proven trusted
- ✓ High performance
- ✓ Optimum spurious noise
- ✓ High dynamic range
- EMI immunity

Cons&Challenges :

- X SWaP
- X Many filters

Down-Conversion/Zero IF



Pros:

- ✓ Maximum ADC bandwidth
- ✓ Simplest wideband option Cons&Challenges:
- X Image rejection (I/Q balance)
- old X In-band IF harmonics
- X EMI immunity (IP2)
- X DC and 1/f noise
- X SWaP

Direct Sampling



Pros:

- ✓ Simple architecture
- ✓ No mixer

Cons&Challenges :

- X ADC input bandwidth must be high
- X Gain not distributed across frequency
- ★ ADC DC power maybe high







EV10AS940, one of the fastest possible ADC @ 10bit. Main Features:

Max Sampling frequency (Fs): 12.8 GSPS.

BW(-3dB) 35GHz

Power 2.5W @12.8 GHz

SFDR 55dB up to 35GHz











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SFDR

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Bandpass Filter, total band to cover 15...25 GHz

Divided into Sub-Bands (SB)







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Cheby is selected. **Goals & Constraints:** Determine order N (odd orders are prefered) Insertion loss IL **Quality factor Q**

Python modules are developed

...



Colorbar: -60 dB rejection BW cheby1, Bandpass: 15.0-17.5GHz, (Frequency(-60dB) |rejection BW)[X:Undersampling impossible] (max Samp. freq[GHz]})

4	11.6 11.0	11.7 10.8	11.8 10.5	11.8 10.4	11.9 10.2	11.9 10.1	12.0 9.9	12.0 9.8	12.1 9.7	12.1 9.6	12.1 9.5	12.2 9.4	12.2 9.3	12.2 9.3	12.2 9.2			
	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X			
ĿO -	13.0 7.3	13.0 7.1	13.1 7.0	13.1 6.9	13.1 6.9	13.2 6.8	13.2 6.7	13 2/6.7	13.2 6.6	13.3 6.5	13.3 6.5	13.3 6.5	13.3 6.4	13.3 6.4	13.3 6.3			
	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X			
order	13.6 5.6	13.7 5.5	13.7 5.4	13.7 5.4	13.8 5.3	13.8 5.3	13.8 5.2	13.8 5.2	13.8 5.2	13.8 5.1	13.8 5.1	13.9 5.1	13.9 5.1	13.9 5.0	13.9 5.0			
6	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X			
Filter	14.0 4.7	14.1 4.6	14.1 4.6	14.1 4.5	14.1 4.5	14.1 4.5	14.1 4.4	14.1 4.4	14.2 4.4	14.2 4.4	14.2 4.3	14.2 4.3	14.2 4.3	14.2 4.3	14.2 4.3			
7	√(12.5)	√(12.4)	√(12.4)	√(12.4)	√(12.4)	√(12.4)	√(12.4)	~(12.4)	~(12.4)	√(12.4)	√(12.3)	√(12.3)	√(12.3)	√(12.3)	√(12.3)			
co -	14.3 4.1	14.3 4.1	14.3 4.0	14.3 4.0	14.3 4.0	14.3 4.0	14.3 3.9	14.4 3.9	14.4 3.9	14.4 3.9	14.4 3.9	14.4 3.9	14.4 3.8	14.4 3.8	14.4 3.8			
	√(12.3)	√(12.2)	√(12.2)	√(12.2)	√(12.2)	√(12.2)	√(12.2)	~(12.2)	√(12.2)	√(12.2)	√(12.2)	√(12.2)	√(12.2)	√(12.2)	√(12.2)			
6	14.4 3.7	14.4 3.7	14.5 3.7	14.5 3.7	14.5 3.7	14.5 3.6	14.5 3.6	14.5 3.6	14.5 3.6	14.5 3.6	14.5 3.6	14.5 3.6	14.5 3.5	14.5 3.5	14.5 3.5			
	√(12.1)	√(12.1)	∽(12.1)	√(12.1)	∽(12.1)	√(12.1)	(9.1)	√(9.1)	∽(9.0)	√(9.0)	∽(9.0)	√(9.0)	∽(9.0)	∽(9.0)	✓(9.0)			
	0.5	0.6 es ·s	0.7 50	0.8	0.9	1.0	1.1 R	1.2 ipple level c	1.6	1.7	1.8	1.9 /D SCHOOL OF						
Univ	Hau d ersity of Applic	ute Ecole Spéci le Suisse occid ed Sciences an	ialisée entale d Arts				9											

Western Switzerland



Q₀ is calculated using Dishal's method

$$IL(f_c) = \frac{4.343f_c}{\Delta f Q_u} \sum_{i=1}^N g_i \, \mathrm{dB}$$





(b) Type 2

SCHOOL OF

AND

ENGINEERING

MANAGEMENT

Calc IL dB @ **f**₀=16.25, BW=2.5 GHz and rp of Chebyshev circuit = 1 dB

										Unloa	ided Q										
	10.0	114.7	219.5	324.2	428.9	533.7	638.4	743.2	847.9	952.6	1057.4	1162.1	1266.8	1371.6	1476.3	1581.1	1685.8	1790.5	1895.3	2000.0	0.0
4	57.7	5.0	2.6	1.8	1.3	1.1	0.9	0.8	0.7	0.6	0.5	0.5	0.5	0.4	0.4	0.4	0.3	0.3	0.3	0.3	0.2
i≓ ∽	54.7	4.8	2.5	1.7	1.3	1.0	0.9	0.7	0.6	0.6	0.5	0.5	0.4	0.4	0.4	0.3	0.3	0.3	0.3	0.3	- 0.2
e e	45.0	3.9	2.1	1.4	1.0	0.8	0.7	0.6	0.5	0.5	0.4	0.4	0.4	0.3	0.3	0.3	0.3	0.3	0.2	0.2	-0.4
	42.1	3.7	1.9	1.3	1.0	0.8	0.7	0.6	0.5	0.4	0.4	0.4	0.3	0.3	0.3	0.3	0.2	0.2	0.2	0.2	-0.6
a er	32.4	2.8	1.5	1.0	0.8	0.6	0.5	0.4	0.4	0.3	0.3	0.3	0.3	0.2	0.2	0.2	0.2	0.2	0.2	0.2	-0.8
ດ -	29.6	2.6	1.3	0.9	0.7	0.6	0.5	0.4	0.3	0.3	0.3		0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.1	1.0
								~ ~													10

Calc IL dB @ f₀=16.25, BW=2.5 GHz and rp of Chebyshev circuit = 1.5 dB

6	33.1	2.9	1.5	1.0	0.8	0.6	0.5	0.4	0.4	0.3	0.3	0.3	0.3	0.2	0.2	0.2	0.2	0.2	0.2	0.2	1.0
8 e	34.9	3.0	1.6	1.1	0.8	0.7	0.5	0.5	0.4	0.4	0.3	0.3	0.3	0.3	0.2	0.2	0.2	0.2	0.2	0.2	-0.8
ord	46.4	4.0	2.1	1.4	1.1	0.9	0.7	0.6	0.5	0.5	0.4	0.4	0.4	0.3	0.3	0.3	0.3	0.3	0.2	0.2	-0.6
e e	48.3	4.2	2.2	1.5	1.1	0.9	0.8	0.6	0.6	0.5	0.5	0.4	0.4	0.4	0.3	0.3	0.3	0.3	0.3	0.2	-0.4
n <u>∏</u>	59.8	5.2	2.7	1.8	1.4	1.1	0.9	0.8	0.7	0.6	0.6	0.5	0.5	0.4	0.4	0.4	0.4	0.3	0.3	0.3	-0.2
4	61.7	5.4	2.8	1.9	1.4	1.2	1.0	0.8	0.7	0.6	0.6	0.5	0.5	0.4	0.4	0.4	0.4	0.3	0.3	0.3	
	10.0	114.7	219.5	324.2	428.9	533.7	638.4	743.2	847.9	952.6	1057.4	1162.1	1266.8	1371.6	1476.3	1581.1	1685.8	1790.5	1895.3	2000.0	-0.0
										Unloa	ided Q										

$Q_0>400 \rightarrow CavitySurfaces+losses of moving elements$

Hes∙so

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Specification of All SBs

R = 1 dB		A _r = 60 dB																	
	19	t band-pa	ISS			2n	d band-pa	ass			Зr	d band-pa	ISS			4t			
	f _p : 15	GHz f _{p+} : 13	7.5 GHz			f _p : 17.5	GHz f _{p+} : 2	20.0 GHz			f _{p-} : 20.0	GHz f _{p+} : 2	2.5 GHz			f _p .: 22.5 GHz f _{p+} : 25.0 GHz			
N-Orde	der F _{r-} F _{r+} B _r Min FS				F _{r-}	F _{r+}	Br	Min FS		F _{r-}	F _{r+}	Br	Min FS		F _{r-}	F _{r+}	Br	Min FS	
4	11.936	21.992	10.056	-	4	14.344	24.4	10.056	-	4	16.773	26.829	10.056	-	4	19.216	29.272	10.056	-
5	13.161	19.945	6.7833	-	5	15.622	22.405	6.7832	-	5	18.091	24.875	6.7836	-	5	20.566	27.351	6.7845	-
6	13.775	19.056	5.2815	-	6	16.253	21.534	5.2816	-	6	18.736	24.018	5.2817	-	6	21.223	26.506	5.2827	-
7	14.124	18.586	4.4624	12.391	7	16.609	21.071	4.4623	-	7	19.098	23.562	4.4641	11.781	7	21.59	26.052	4.4627	-
8	14.341	18.305	3.9642	12.203	8	16.831	20.795	3.9639	10.397	8	19.324	23.289	3.9653	11.645	8	21.817	25.784	3.9673	10.314
9	14.485	18.122	3.6369	12.081	9	16.977	20.614	3.6363	10.307	9	19.472	23.111	3.6389	9.2445	9	21.967	25.608	3.641	8.5359
						<u> </u>													

R = 1.5 dB $A_r = 60 dB$

	1s	t band-pa	ISS			2nd band-pass					3rd band-pass					4th band-pass			
	f _p : 15 (GHz f _{p+} : 1	7.5 GHz			f _p : 17.5	GHz f _{p+} : 2	20.0 GHz			f _{P-} : 20.0	GHz f _{p+} : 2	22.5 GHz			f _p : 22.5			
N-Order	F _{r-}	F _{r+}	Br	Min FS		F _{r-}	F _{r+}	Br	Min FS		F _{r-}	F _{r+}	Br	Min FS		F _{r-}	F _{r+}	Br	Min FS
4	12.132	21.638	9.5058	-	4	14.55	24.055	9.5054	-	4	16.986	26.492	9.5061	-	4	19.436	28.942	9.5062	-
5	13.276	19.773	6.4967	-	5	15.74	22.237	6.4968	-	5	18.212	24.709	6.4968	-	5	20.69	27.187	6.4978	-
6	13.849	18.955	5.1056	-	6	16.329	21.435	5.1054	-	6	18.813	23.92	5.1066	-	6	21.3	26.407	5.1067	-
7	14.176	18.518	4.3422	12.345	7	16.663	21.006	4.3429	-	7	19.153	23.495	4.3421	11.748	7	21.644	25.989	4.3451	-
8	14.379	18.256	3.8765	12.17	8	16.87	20.747	3.8769	10.373	8	19.362	23.241	3.8788	11.621	8	21.859	25.736	3.8771	10.294
9	14.516	18.083	3.5671	9.0417	9	17.008	20.579	3.5711	10.289	9	19.502	23.075	3.573	9.2299	9	21.999	25.572	3.5728	8.524



















VARIABLE Passband filtering for undersampling ADCs

- Band to be covered 15-25GHz
- Or better 15-30GHz=1 octave (1:2 ratio) =WIDE band!
- Most «tunable filters» +-5% with standard methods: adjustable to some fixed specification
- → we need to get back to basics and «make it move»
- → we need an actuator
- ➡ fortunately we have one from a biomedical project



- Miniature step motor, Distance resolution ~0.1um/step! will be sufficient
- Lots of other technological challenges (sliding contacts at 20GHz???)







- Filter requirements, type and topology are determined.
- Filter architecture is chosen
- Using a wide band & Fast ADC
- Tunable design(possibility to switch between SBs).







Contacts

Mohammad Reza Khalvati mohammad.khalvati@heig-vd.ch

SKACH Instrumentation Program chair: Dominique Bovey (HEIG-VD) <u>dominique.bovey@heig-vd.ch</u> +41 24 557 27 54 / +41 79 327 71 53

HES-SO-level administration/coordination () SKACH board member for HES-SO Evelina Breschi <u>evelina.breschi@hes-so.ch</u> Phone: +41 58 900 01 12

HEIG-VD-level administrative contact: Pascal Coeudevez pascal.coeudevez@heig-vd.ch +41 24 557 27 61







Goal: How to couple cells effectively (to achieve a sufficient coupling level)





